

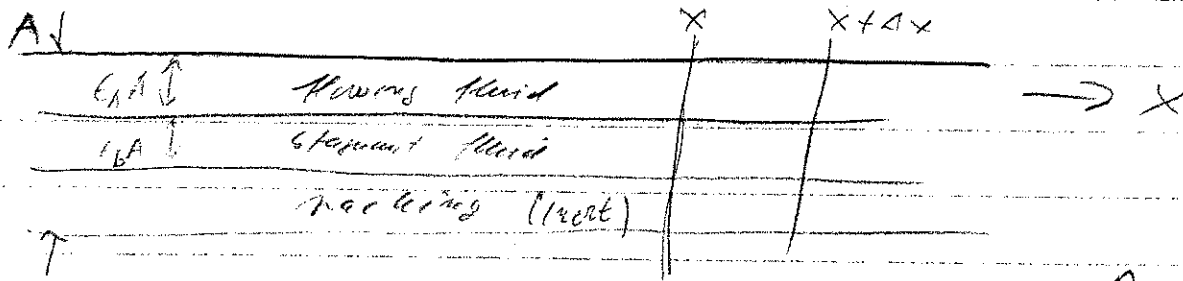
Consider cross flow model for packed bed

A = total cross sectional area

$\epsilon_a A$ = cross sectional area for flowing fluid

$\epsilon_b A$ = cross sectional area of stagnant fluid

$(\epsilon_a + \epsilon_b) A = \epsilon A =$ total fluid occupied cross sectional area



$$u_a = \text{mean actual velocity} = \frac{Q}{\epsilon_a A}$$

$$\bar{t} = \frac{\epsilon A L}{Q} = \frac{\epsilon V}{Q} = \frac{\epsilon A L}{u_a \epsilon_a A} = \frac{\epsilon}{\epsilon_a} \frac{L}{u_a} = \frac{\epsilon L}{\bar{u}}$$

$$\bar{u} = \text{superficial velocity} = \frac{Q}{A} = \epsilon_a u_a$$

$$u_i = \text{interstitial velocity} = \frac{Q}{\epsilon A} = \frac{\epsilon_a u_a}{\epsilon} = \frac{\bar{u}}{\epsilon}$$

$$u_a \epsilon_a A C_1 \Big|_x - u_a \epsilon_a A C_1 \Big|_{x+\Delta x} - f A \Delta x (C_1 - K C_2) = \epsilon_b A \frac{\partial C_1}{\partial t} + R_1 \epsilon_b A \Delta x$$

$f \left(\frac{\text{m}^3}{\text{m}^3 \cdot \text{s}} \right)$ = exchange flow rate per unit volume of total bed (voids active + inactive fluid)

$$\epsilon_b A \Delta x + f A \Delta x (C_1 - K C_2) = \epsilon_b A \frac{\partial C_2}{\partial t}$$

$R_1 \left(\frac{\text{mol}}{\text{m}^3 \cdot \text{s}} \right)$ - rate of formation of species 1 (C_1) per unit volume of active fluid (in active region)

$R_2 \left(\frac{\text{mol}}{\text{m}^3 \cdot \text{s}} \right)$ - rate of formation of species 2 (C_2) per unit volume of ~~active~~ fluid (in inactive region)

Typically we assume $K = 1 \left(\frac{\text{mol/m}^3 \text{ a. fluid}}{\text{mol/m}^3 \text{ s. fluid}} \right)$

If $R \left(\frac{\text{mol}}{\text{m}^3 \text{ bed s}} \right)$ then $\frac{R}{\epsilon} \left(\frac{\text{mol}}{\text{m}^3 \text{ fluid s}} \right)$ ←
 $R_1 = R_2 = \frac{R}{\epsilon}$ ←

$$-u_0 \epsilon_a \frac{\partial C_1}{\partial x} - f(C_1 - C_2) + R \frac{\epsilon_a}{\epsilon} = \epsilon_a \frac{\partial C_1}{\partial t}$$

$$f(C_1 - C_2) + R \frac{\epsilon_b}{\epsilon} = \epsilon_b \frac{\partial C_2}{\partial t}$$

$$t=0; \quad C_1 = C_2 = 0 \quad ; \quad x=0 \quad ; \quad C_1 = C_0$$

Recall $u_0 \epsilon_a = \bar{u}$

Let $y = \frac{dp}{dp}$; $\gamma_1 = \frac{C_1}{C_0}$; $\gamma_2 = \frac{C_2}{C_0}$

$$- \frac{\bar{u} C_0}{dp} \frac{\partial \gamma_1}{\partial y} - f C_0 (\gamma_1 - \gamma_2) + \frac{\epsilon_a}{\epsilon} R = \epsilon_a C_0 \frac{\partial \gamma_1}{\partial t}$$

$$f C_0 (\gamma_1 - \gamma_2) + R \frac{\epsilon_b}{\epsilon} = \epsilon_b C_0 \frac{\partial \gamma_2}{\partial t}$$

$$- \frac{\partial \gamma_1}{\partial y} - \frac{f dp}{\bar{u}} (\gamma_1 - \gamma_2) + \frac{\epsilon_a}{\epsilon} \left(\frac{dp}{dp} R \right) = \left(\frac{dp}{\bar{u} \epsilon} \right) \frac{\partial \gamma_1}{\partial t}$$

Let $\epsilon = \frac{\bar{u} dp}{dp \epsilon}$; $S = \frac{\epsilon_b}{\epsilon}$; $\bar{R} = \frac{dp}{\bar{u} C_0} R$; $F = \frac{f dp}{\bar{u}}$

$$- \frac{\partial \gamma_1}{\partial y} - F (\gamma_1 - \gamma_2) + (1-S) \bar{R} = (1-S) \frac{\partial \gamma_1}{\partial \epsilon}$$

$$\frac{f dp}{\bar{u}} (\gamma_1 - \gamma_2) + \frac{dp}{\bar{u} C_0} R \frac{\epsilon_b}{\epsilon} = \frac{\epsilon_b dp}{\bar{u} \epsilon} \frac{\partial \gamma_2}{\partial t}$$

$$F (\gamma_1 - \gamma_2) + S \bar{R} = S \frac{\partial \gamma_2}{\partial \epsilon}$$

$$t=0 \quad \gamma_1 = \gamma_2 = 0$$

$$y = \frac{L}{dp} \quad \gamma_1 = \gamma_{max}$$

$$x=0 \quad u = \dots$$

TWO cases are of interest.

Steady state reactor model: catalyst
two parameters F and S .

Transient model yielding the
 E -curve.

Let us get F and S from
known information about reactor tests.

The Ergun equation for pressure
drop is:

$$-\frac{dp}{dz} = \frac{150 \mu (1-\epsilon)^2 \bar{u}}{\epsilon^3 d_p^2} + 1.75 \left(\frac{1-\epsilon}{\epsilon^3} \right) \frac{\rho \bar{u}^2}{d_p}$$

$$dp = \frac{6}{5V}$$

We hypothesize (Kunii et al.) that
the second term is due to turbulent
wake phenomena caused by the
momentum exchange between the
flowing and stagnant phase.

Momentum balance flow fields

$$-\epsilon_a \left(\frac{dp}{dz} \right)' = f \rho \frac{\bar{u}}{\epsilon_a}$$

$$-\left(\frac{dp}{dz} \right)' = f \rho \frac{\bar{u}}{\epsilon_a^2} = 1.75 \left(\frac{1-\epsilon}{\epsilon^3} \right) \frac{\rho \bar{u}^2}{d_p}$$

$$\frac{f d_p}{\bar{u}} = 1.75 \left(\frac{1-\epsilon}{\epsilon} \right) \left(\frac{\epsilon_a}{\epsilon} \right)^2$$

$$F = 1.75 \left(\frac{1-\epsilon}{\epsilon} \right) (1-S)^2$$

We determine now the second parameter from the variance of the variable response (the spread of the curve around the mean is related to the standard deviation etc).

We need to solve:

$$-\frac{\partial \delta_1}{\partial g} - F(\delta_1, -\delta_2) = (1-s) \frac{\partial \delta_1}{\partial \tau}$$

$$F(\delta_1, -\delta_2) = s \frac{\partial \delta_2}{\partial \tau}$$

$$\tau = 0 \quad \delta_1 = \delta_2 = 0 \quad ; \quad g = 0 \quad \delta_1 = s/\tau$$

Laplace transform of the above yields

$$\text{with } \bar{\delta}_1 = \mathcal{L}\{\delta_1\}, \quad \bar{\delta}_2 = \mathcal{L}\{\delta_2\} = \int_0^\infty e^{-\tau t} \delta_2 dt$$

$$\frac{d\bar{\delta}_1}{dg} = -F(\bar{\delta}_1, -\bar{\delta}_2) - (1-s)s\bar{\delta}_1$$

$$F(\bar{\delta}_1, -\bar{\delta}_2) = s s \bar{\delta}_2 \quad (\text{all } \underline{0=0})$$

Hence

$$\bar{\delta}_2 = \frac{F\bar{\delta}_1}{F + s s}$$

$$\bar{\delta}_1 - \bar{\delta}_2 = \frac{s s \bar{\delta}_1}{F + s s}$$

so that

$$\frac{d\bar{\delta}_1}{dg} = - \left[\frac{F s s}{F + s s} + (1-s)s \right] \bar{\delta}_1$$

$$g = 0 \quad \bar{\delta}_1 = 1$$

$$\bar{y}_1 = e^{-\left[\frac{FS_0}{F+S_0} + (1-S)_0\right]y} = e^{-\frac{FS_0}{F+S_0} + (1-S)_0 y}$$

we are interested in the variance
 transition of the exit concentration

$$\bar{y}_1(y = \frac{L}{d_0}) \quad \text{which is}$$

$$\bar{y}_{\text{EXIT}} = e^{-\frac{L}{d_0} \left[\frac{FS_0}{F+S_0} + (1-S)_0 \right]} \quad (*)$$

Since we want the variance we need to
 expand the above to small values of s .

$$\begin{aligned} \bar{y}_{\text{EXIT}} &= e^{-\frac{L}{d_0} \left[F - \frac{F}{1+(S/F)_0} + (1-S)_0 \right]} \\ &= e^{-\frac{L}{d_0} \left[F - F \left(1 - \frac{S}{F} + \frac{S^2}{F^2} - \frac{S^3}{F^3} \right) + s - s_0 \right]} \\ &= e^{-\frac{L}{d_0} \left[s - \frac{S^2}{F} s^2 + \frac{S^3}{F^2} s^3 - \dots \right]} \\ &= e^{-\frac{L}{d_0} s \left[1 - \frac{S^2}{F} s + \frac{S^3}{F^2} s^2 - \dots \right]} \\ &= 1 - \frac{L}{d_0} s \left[1 - \frac{S^2}{F} s + \frac{S^3}{F^2} s^2 \right] + \frac{L^2}{2d_0^2} s^2 \left[1 - \frac{S^2}{F} s \right]^2 \\ &= 1 - \frac{L}{d_0} s + \left[\frac{S^2 L}{F d_0} + \frac{1}{2} \left(\frac{L}{d_0} \right)^2 \right] s^2 - o(s^2) \end{aligned}$$

Compare with

$$\bar{y}_{\text{EXIT}} = \mu_0 - \mu_1 s + \frac{\mu_2}{2} s^2 - \frac{\mu_3}{6} s^3 \dots$$

yields

$$\mu_0 = 1$$

$$\mu_1 = \frac{L}{d_0}$$

$$\mu_2 = 2 \left[\frac{S^2 L}{F d_0} + \frac{1}{2} \left(\frac{L}{d_0} \right)^2 \right]$$

We require that $\bar{F}(z)$ is normal $\bar{E}(z)$ or $\bar{E}_0(z)$ since $\tau = \frac{\bar{u}t}{\epsilon dp}$ while

$$\theta = \frac{\bar{u}t}{\epsilon L} = \tau \left(\frac{dp}{L} \right)$$

$$\bar{\theta} = \int_0^{\infty} \theta E_\theta(\theta) d\theta = \left(\frac{dp}{L} \right) \int_0^{\infty} \tau E_\theta(\theta) d\theta = \left(\frac{dp}{L} \right) \left(\frac{L}{dp} \right) = 1 \text{ a.u.}$$

$$\begin{aligned} \sigma_\theta^2 &= \int_0^{\infty} (\theta - 1)^2 E_\theta(\theta) d\theta = \left(\frac{dp}{L} \right)^2 \int_0^{\infty} \left(\tau - \frac{L}{dp} \right)^2 E_\theta(\theta) d\theta \\ &= \frac{\int_0^{\infty} \left(\tau - \frac{L}{dp} \right)^2 E_\theta(\theta) d\theta}{\left(L/dp \right)^2} = \frac{\sigma_\tau^2}{\mu_1^2} = \frac{\mu_2 - \mu_1^2}{\mu_1^2} \end{aligned}$$

Thus

$$\sigma_\theta^2 = \frac{2 \frac{S^2}{F} \frac{L}{dp} + \left(\frac{L}{dp} \right)^2 - \left(\frac{L}{dp} \right)^2}{\left(\frac{L}{dp} \right)^2} = \frac{2 S^2/F}{(L/dp)}$$

$$\sigma_\theta^2 = \frac{2 S^2}{F L} \left(\frac{dp}{L} \right)$$

Now we know from before (see)

$$\sigma_\theta^2 = \frac{2}{Pe_z} = \frac{2 E_z}{\bar{u} L} = \frac{2 E_z}{\bar{u} dp} \left(\frac{dp}{L} \right)$$

$$\text{Let } \frac{\bar{u} dp}{E_z} = Bo = Pe_{eff}$$

$$Bo = f(Pe) \quad Pe = 100 \quad \underline{\underline{Bo = 2}}$$

Equating the two we get

$$\frac{S^2}{F} \left(\frac{dp}{L} \right) = \frac{1}{Bo} \left(\frac{dp}{L} \right)$$

$$\frac{S^2}{F} = \frac{1}{Bo}$$

$$\text{or } \boxed{F = S^2 Bo}$$

$$S^2 B_0 = 1.75 \left(\frac{1-\epsilon}{\epsilon} \right) (1-S)^2$$

$$\frac{S}{1-S} = \sqrt{\frac{1.75}{B_0} \left(\frac{1-\epsilon}{\epsilon} \right)}$$

$$S = \frac{\sqrt{\frac{1.75}{B_0} \left(\frac{1-\epsilon}{\epsilon} \right)}}{1 + \sqrt{\frac{1.75}{B_0} \left(\frac{1-\epsilon}{\epsilon} \right)}}$$

$$F = \frac{1.75 \left(\frac{1-\epsilon}{\epsilon} \right)}{\left[1 + \sqrt{\frac{1.75}{B_0} \left(\frac{1-\epsilon}{\epsilon} \right)} \right]^2}$$

Typically

$$B_0 = 2$$

$$\epsilon = 0.5$$

$$S \approx 0.342$$

$$F \approx 0.467$$

The steady state model to be solved

is

$$\frac{d\delta_1}{dz} = -F(\delta_1 - \delta_2) + (1-S)\bar{R}|_{\delta_1} \quad (1)$$

$$F(\delta_1 - \delta_2) + S\bar{R}|_{\delta_2} = 0 \quad (2)$$

$$y=0, \quad \delta_1 = 1$$

$$\delta_{exit} = \delta_1 \left(y = \frac{z}{L} \right)$$

where \bar{R} is the dimensionless rate of formation

for an m -th order reaction

$$R = kC^m$$

$\frac{\text{mol}}{\text{m}^3 \cdot \text{bed}}$

$$\bar{R} = \frac{d_p}{4C_{10}} kC^m = \frac{d_p k C_{10}^{m-1}}{4} \delta_1^m$$

$$\text{Let } Da_p = \frac{d_p k C_{10}^{m-1}}{4}$$

The rate will (for a catalytic reaction) normally be given by:

$$R_f = k_f C^m$$

$\frac{\text{mol}}{\text{m}^3 \cdot \text{m} \cdot \text{s}}$

$$k_f \epsilon = k$$

Consider 1st order reaction

$$D_{ep} = \frac{dD}{dt} k$$

The solution is given by (W40?)

$$S_{cont} = e^{-\left[\frac{FS D_{ep}}{F + S D_{ep}} + (1-S) D_{ep} \right] \frac{L}{dP}}$$

In the limit if there is no exchange

$$F = 0$$

$$S_{cont} = e^{-(1-S) D_{ep} \frac{L}{dP}} = e^{-(1-S) k \frac{L}{dP}}$$

~~$$= e^{-\left(\frac{S_1}{1-S} \right) k \frac{L}{dP}}$$~~

QED

For nonlinear rate forms we would have to solve the nonlinear eq (2) at each step in y . Instead solve (2) at $y=0$ to get S_{20} from the solution of

$$F(1 - S_{20}) + S \bar{R}(S_{20}) = 0$$

Then differentiate eq (2)

$$F \frac{dS_1}{dy} - F \frac{dS_2}{dy} + S \frac{d\bar{R}}{dS_2} \frac{dS_2}{dy} = 0$$

$$\left(F - S \frac{d\bar{R}}{dS_2} \right) \frac{dS_2}{dy} = F \frac{dS_1}{dy} = -F^2 (1 - S_{20}) + F(1-S) \bar{R}$$

Integrate simultaneously for $y = \frac{L}{dP}$

Let us find the impulse response

$$\begin{aligned}\bar{y}_{\text{exit}} &= e^{-\left[\frac{FS^2}{F+S^2} + (1-S)^2\right] \frac{L}{d_p}} \\ &= e^{-\frac{L}{d_p} \left[F - \frac{F^2/S}{S + (F/S)} + (1-S)^2 \right]} \\ &= \underbrace{e^{-\frac{L}{d_p} F}}_{\text{constant}} \underbrace{e^{-\frac{L}{d_p} (1-S)^2}}_{\text{time lag}} e^{\frac{L}{d_p} (F^2/S) / (S + F/S)}\end{aligned}$$

Let $\bar{f}(s) = e^{\frac{L}{d_p} (F^2/S) / (S + F/S)}$

$$\bar{y}_{\text{exit}} = e^{-\frac{L}{d_p} F} e^{-\frac{L}{d_p} (1-S)^2} \cdot \bar{f}(s)$$

$$y_{\text{exit}} = e^{-\frac{L}{d_p} F} \int_0^{\infty} f(\tau) \delta\left(\tau - \frac{L}{d_p} (1-S)^2\right) d\tau$$

$$= e^{-\frac{L}{d_p} F} f\left(\tau - \frac{L}{d_p} (1-S)^2\right) H\left(\tau - \frac{L}{d_p} (1-S)^2\right)$$

Consider $\bar{f}(s) = e^{\frac{L}{d_p} (F^2/S) / (S + F/S)} = \bar{g}\left(s + \frac{F}{S}\right)$

Rule 1 $\mathcal{L}^{-1}\{\bar{g}(s+a)\} = e^{-at} \mathcal{L}^{-1}\{\bar{g}(s)\}$

where $\bar{g}(s) = e^{\frac{L}{d_p} (F^2/S) / s}$

Rule 2: $\mathcal{L}^{-1}\{e^{\alpha/s} - 1\} = \sqrt{\frac{\alpha}{\pi}} I_1(2\sqrt{\alpha t})$

Hence

$$\mathcal{L}^{-1}\{e^{\alpha/s}\} = \delta(t) + \sqrt{\frac{\alpha}{\pi}} I_1(2\sqrt{\alpha t})$$

$$\alpha = \frac{F^2 L}{S d_p}$$

Therefore

$$\mathcal{L}^{-1} \left\{ e^{\frac{L}{dp}(F^2/s)/s} \right\} = \delta(\tau) + \sqrt{\frac{FL}{s^2 dp}} I_1 \left(2\sqrt{\frac{F^2}{s} \frac{L}{dp}} \right) = g(\tau)$$

$$\mathcal{L}^{-1} \left\{ e^{\frac{L}{dp}(F^2/s)/(s+F/s)} \right\} = e^{-\frac{FL}{s}} \left\{ \delta(\tau) + \frac{F}{\sqrt{s^2 \frac{L}{dp}}} I_1 \left(2F \sqrt{\frac{L}{s^2 dp}} \right) \right\}$$

Finally

$$g_{\text{exit}}(\tau) = e^{-\frac{LF}{dp}} e^{-\frac{FL}{s}(\tau - (1-s))} \left\{ \delta(\tau - (1-s)) + \frac{F}{\sqrt{s^2 \frac{L}{dp} (1-s)}} I_1 \left(2F \sqrt{\frac{L(1-s)}{dp s}} \right) \right\} H(\tau - (1-s))$$

$$g_{\text{exit}}(\tau) d\tau = E_0(\theta) d\theta = E(t) dt$$

$$\theta = \frac{\bar{u}}{cL} \tau = \left(\frac{dp}{L}\right) \tau \quad \tau = \frac{L}{dp} \theta$$

$$E_0(\theta) = \left(\frac{L}{dp}\right) g_{\text{exit}}$$

$$E(t) = \frac{1}{L} E_0(\theta)$$

$$E_0(\theta) = e^{-\frac{LF}{dp}} e^{-\frac{FL}{dp s}(\theta - (1-s))} \left\{ \frac{L}{dp} \delta(\theta - (1-s)) + \right.$$

$$\left. + \frac{F \frac{L}{dp}}{\sqrt{s(\theta - (1-s))}} I_1 \left(2F \frac{L}{dp} \sqrt{\frac{\theta - (1-s)}{s}} \right) \right\} H(\theta - (1-s))$$

$$E(t) = e^{-\frac{LF}{dp}} e^{-\frac{FL}{dp s} \left(\frac{\bar{u}}{cL} t - (1-s)\right)} \left\{ \frac{L}{dp} \delta\left(\frac{\bar{u}}{cL} t - (1-s)\right) + \right.$$

$$\left. + \frac{F \frac{L}{dp} \frac{1}{L}}{\sqrt{s \left(\frac{\bar{u}}{cL} t - (1-s)\right)}} I_1 \left(2F \frac{L}{dp} \sqrt{\frac{\bar{u}}{cL} \left(\frac{\bar{u}}{cL} t - (1-s)\right)} \right) \right\} H\left(\frac{\bar{u}}{cL} t - (1-s)\right)$$

Krall

$$S = \frac{c_0}{c}$$

$$1-S = \frac{c_0 L}{c}$$

$$F = \frac{f dp}{\bar{u}}$$

$$E(t) = e^{-\frac{fL}{\bar{u}}} e^{-\frac{fLc_0}{\bar{u}c} \left(\frac{\bar{u}}{cL} t - \frac{c_0}{c} \right)} \left\{ \delta \left(t - \frac{c_0 L}{\bar{u}} \right) \right.$$

$$+ \frac{f dp \frac{L}{dp}}{\bar{u} \sqrt{\frac{c_0}{c} \left(\frac{\bar{u} t}{cL} - \frac{c_0}{c} \right)}} I_1 \left(2 \frac{f dp L}{\bar{u} c} \sqrt{\frac{\frac{\bar{u} t}{cL} - \frac{c_0}{c}}{\frac{c_0}{c}}} \right) \Bigg\} \times H \left(t - \frac{c_0 L}{\bar{u}} \right)$$

$$\bar{t} = \frac{cL}{\bar{u}}$$

$$\frac{L}{\bar{u}} = \frac{\bar{t}}{c}$$

$$E(t) = e^{-\frac{f\bar{t}}{c}} e^{-\frac{f\bar{t}}{c_0} \left(\frac{t}{\bar{t}} - \frac{c_0}{c} \right)} \left\{ \frac{L}{dp} \delta \left(t - \frac{c_0}{c} \bar{t} \right) \right.$$

$$+ \frac{f \bar{t} \frac{dp}{L} \times \frac{L}{dp}}{\sqrt{\frac{c_0}{c} \left(\frac{t}{\bar{t}} - \frac{c_0}{c} \right)}} I_1 \left(2 \frac{f \bar{t}}{c} \sqrt{\frac{\frac{t}{\bar{t}} - \frac{c_0}{c}}{\frac{c_0}{c}}} \right) \Bigg\} H \left(t - \frac{c_0}{c} \bar{t} \right)$$

$$E(t) = e^{-\frac{f\bar{t}}{c}} e^{-\frac{f}{c_0} \left(t - \frac{c_0}{c} \bar{t} \right)} \left\{ \delta \left(t - \frac{c_0}{c} \bar{t} \right) \right.$$

$$+ \frac{f \bar{t}}{c \sqrt{\frac{c_0}{c} \left(\frac{t}{\bar{t}} - \frac{c_0}{c} \right)}} I_1 \left(2 f \frac{\bar{t}}{c} \sqrt{\frac{t - \frac{c_0}{c} \bar{t}}{\frac{c_0}{c} \bar{t}}} \right) \Bigg\}$$

900

$H \left(t - \frac{c_0}{c} \bar{t} \right)$

Old solution

A-10

$$E(t) = e^{-\alpha} e^{-\frac{\alpha}{1-\rho} t} \left\{ \delta(t - \rho \bar{t}) + \frac{\alpha}{\sqrt{(1-\rho) \bar{t}} (t - \rho \bar{t})} I_1 \left(2\alpha \sqrt{\frac{t - \rho \bar{t}}{(1-\rho) \bar{t}}} \right) \right\} H(t - \rho \bar{t})$$

$$\frac{c_0}{c} = \beta = 1 - s$$

$$\alpha = \frac{f \bar{t}}{c}$$

$$1 - \rho = \frac{c_0}{c} = s$$

$$E(t) = e^{-\frac{f \bar{t}}{c}} e^{-\frac{f}{c_0} (t - \frac{c_0}{c} \bar{t})} \left\{ \delta \left(t - \frac{c_0}{c} \bar{t} \right) \right.$$

$$+ \frac{f \bar{t}}{c \sqrt{\frac{c_0}{c} \bar{t}} (t - \frac{c_0}{c} \bar{t})} I_1 \left(2 \frac{f \bar{t}}{c} \sqrt{\frac{t - \frac{c_0}{c} \bar{t}}{\frac{c_0}{c} \bar{t}}} \right) \left. \right\} H \left(t - \frac{c_0}{c} \bar{t} \right)$$

$$+ \frac{f}{c \sqrt{\frac{c_0}{c} \left(\frac{t}{c} - \frac{c_0}{c} \right)}}$$

QED