

**ChE 512 General Population Balance**

Consider a medium in Eulerian space consisting of an assembly of entities.

$\psi(x_1, x_2, x_3, \zeta_1, \zeta_2, \zeta_m)$  - probability density function (pdf) of an ensemble of entities

$x_1, x_2, x_3$  - spatial coordinates

$\zeta_i$  - i-th property of the entity (size, age, surface area, activity, etc.)

$i = 1, 2 \dots m$

$\psi dx_1 dx_2 dx_3 d\zeta_1 d\zeta_2 \dots d\zeta_m$  - (mass) fraction of the population contained around the point

$x_1, x_2, x_3$  with properties in the neighborhood of  $\zeta_1, \zeta_2, \dots, \zeta_m$

$$\int_{R_m} \psi dx_1 dx_2 dx_3 d\zeta_1 d\zeta_2 \dots d\zeta_m = 1$$

$\psi$  is number pdf (density) of the population.

We deal now with  $m+3$  dimensional space.

Define

$$B = \frac{\text{birth of entities}}{(\text{unit time})(\text{unit geometric volume})(\text{unit property change})}$$

$$D = \frac{\text{death of entities}}{(\text{unit time})(\text{unit geometric volume})(\text{unit property change})}$$

Pick an arbitrary (volume) element in the  $(m + 3)$  D space  $\mathfrak{R}(t)$

The conservation law requires

$$\frac{d}{dt} \int_{\mathfrak{R}(t)} \psi d\mathfrak{R} = \int_{\mathfrak{R}(t)} (B - D) d\mathfrak{R}$$

Now relate the "volume" element  $d\mathfrak{R}$  at present to the volume element  $dR$  in some fixed reference configuration.

Recall that (Reynolds Transport Theorem)  $d\mathfrak{R} = J dR$  where

$J = \det F_{iA}$  Jacobian of the transform

$$d\mathfrak{R} = dx_1 dx_2 dx_3 d\zeta_1 d\zeta_2 \dots d\zeta_m$$

$$dR = dX_1 dX_2 dX_3 dZ_1 dZ_2 \dots dZ_m$$

$$J = \frac{\partial(x_1, x_2, x_3, \zeta_1, \dots, \zeta_m)}{\partial(X_1, X_2, X_3, Z_1, \dots, Z_m)} = \begin{vmatrix} \frac{\partial x_1}{\partial X_1} & \frac{\partial x_2}{\partial X_1} & \frac{\partial x_3}{\partial X_1} & \frac{\partial \zeta_1}{\partial X_1} & \dots & \frac{\partial \zeta_m}{\partial X_1} \\ \frac{\partial x_1}{\partial X_2} & \frac{\partial x_2}{\partial X_2} & \frac{\partial x_3}{\partial X_2} & \frac{\partial \zeta_1}{\partial X_2} & \dots & \frac{\partial \zeta_m}{\partial X_2} \\ \dots & \dots & \dots & \dots & \dots & \dots \\ \frac{\partial x_1}{\partial Z_m} & \frac{\partial x_2}{\partial Z_m} & \frac{\partial \zeta_1}{\partial Z_m} & \dots & \frac{\partial \zeta_m}{\partial Z_m} & \dots \end{vmatrix}$$

Thus

$$\begin{aligned} \frac{d}{dt} \int_R \psi J dR &= \int_R (B - D) J dR \\ \int_R \left( \frac{\partial \psi}{\partial t} J + \sum_{i=1}^3 \frac{\partial \psi}{\partial x_i} \frac{dx_i}{dt} J + \sum_{i=1}^m \frac{\partial \psi}{\partial \zeta_i} \frac{d\zeta_i}{dt} J + \psi \frac{dJ}{dt} \right) dR &= \int_R (B - D) J dR \end{aligned}$$

We know that

$$\frac{dJ}{dt} = J \left[ \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z} + \sum_{i=1}^m \frac{\partial V_i}{\partial \zeta_i} \right] = J \left[ \frac{\partial v_1}{\partial x_1} + \frac{\partial v_2}{\partial x_2} + \frac{\partial v_3}{\partial x_3} + \sum_{i=1}^m \frac{\partial V_i}{\partial \zeta_i} \right]$$

where

$$v_i = \frac{dx_i}{dt} - \text{velocity component}$$

$$V_i = \frac{d\zeta_i}{dt} - \text{time rate of change of property } \zeta_i$$

$$\begin{aligned} \int_R J \left\{ \frac{\partial \psi}{\partial t} + \sum_{i=1}^3 V_i \frac{\partial \psi}{\partial x_i} + \sum_{i=1}^m V_i \frac{\partial \psi}{\partial \zeta_i} + \psi \sum_{i=1}^3 \frac{\partial v_i}{\partial x_i} + \psi \sum_{i=1}^m \frac{\partial V_i}{\partial \zeta_i} - B + D \right\} dR &= 0 \\ \int_{\mathfrak{R}(t)} \left\{ \frac{\partial \psi}{\partial t} + \nabla \cdot (\vec{v} \psi) + \sum_{i=1}^m \frac{\partial}{\partial \zeta_i} (V_i \psi) - B + D \right\} d\mathfrak{R} &= 0 \end{aligned}$$

Since choice of  $\mathfrak{R}$  is arbitrary

$$\frac{\partial \psi}{\partial t} + \sum_{i=1}^3 \frac{\partial}{\partial x_i} (\psi v_i) + \sum_{i=1}^m \frac{\partial}{\partial \zeta_i} (\psi V_i) - B + D = 0 \quad (1)$$

is the general microscopic population balance.

Let us now introduce the volume averaged probability density

$$\bar{\psi} \equiv \frac{1}{V} \int_V \psi dV \text{ where } dV = dx_1 dx_2 dx_3$$

Rewrite (1) and assume  $\psi$  independent of position in volume  $V$  except at the surface across which we have the inlet flow,  $S_{in}$  and the surface across which outlet flow occurs,  $S_{out}$ .

$$\begin{aligned} \frac{\partial \psi}{\partial t} + \nabla \cdot (\vec{v} \psi) + \sum_{i=1}^m \frac{\partial}{\partial \zeta_i} (\psi V_i) + D - B &= 0 \quad (1a) \\ \int_V \left[ \frac{\partial \psi}{\partial t} + \nabla \cdot (\vec{v} \psi) \right] dV + \int_V \sum_{i=1}^m \frac{\partial}{\partial \zeta_i} (\psi V_i) dV + \int_V (D - B) dV &= 0 \\ \int_V \nabla \cdot (\vec{v} \psi) dV = \int_S \psi V_n dS = \sum_{i=1}^T v_{ext,i} \psi_{ext,i} S_i + \psi \frac{dV}{dt} \\ V \frac{\partial \bar{\psi}}{\partial t} - Q_{in} \psi_{in} + Q_{out} \psi_{out} + \bar{\psi} \frac{dV}{dt} + V \sum_{i=1}^m \frac{\partial}{\partial \zeta_i} (V_i \bar{\psi}) + V(\bar{D} - \bar{B}) &= 0 \end{aligned}$$

After appropriate mathematical manipulations one gets the following macroscopic population balance

$$\frac{1}{V} \frac{\partial}{\partial t} (\bar{\psi} V) + \sum_{i=1}^m \frac{\partial}{\partial \zeta_i} (\bar{\psi} V_i) + \bar{D} - \bar{B} = \frac{1}{V} (Q_{in} \bar{\psi}_{in} - Q_{out} \bar{\psi}_{out}) \quad (2)$$

where

$$\bar{V}_i = \frac{d\zeta_i}{dt}$$

At steady state

$$\sum_{i=1}^m \frac{\partial}{\partial \zeta_i} (\bar{\psi} \bar{V}_i) + \bar{D} - \bar{B} = \frac{1}{V} (Q_{in} \bar{\psi}_{in} - Q_{out} \bar{\psi}_{out}) \quad (3)$$

Examples:

1. Take

$\zeta_1 = \alpha$  – age of fluid element

$$m = 1$$

steady state  $Q_{in} = Q_{out}$

$$\frac{d}{d\alpha} \left( \bar{\psi} \frac{d\alpha}{dt} \right) + \bar{D} - \bar{B} = \frac{1}{V} (Q_{in} \delta(\alpha) - Q_{out} \bar{\psi}_{out})$$

Let:  $\bar{\psi}(\alpha) = I(\alpha)$       $\bar{\psi}_{out} = E(\alpha)$

$$\frac{dI}{d\alpha} = \frac{1}{t} [\delta(\alpha) - E(\alpha)]$$

$\alpha \Rightarrow \infty$       $I(\alpha) \rightarrow 0$

$$\int_0^{I(\alpha)} dI = \frac{1}{t} \int_0^{\infty} [\delta(\alpha) - E(\alpha)] d\alpha$$

$$I(\alpha) = +\frac{1}{t} \left[ \int_{\alpha}^{\infty} E(\alpha) d\alpha - \int_{\alpha}^{\infty} \delta(\alpha) d\alpha \right] = \frac{1}{t} [1 - F(\alpha)]$$

2. Take  $\zeta_1 = \lambda$  life expectation of fluid element

$$m = 1$$

Steady state  $Q_{in} = Q_{out}$

$$\frac{d}{d\lambda} \left( \bar{\psi} \frac{d\lambda}{dt} \right) + \bar{D} - \bar{B} = \frac{Q}{V} [\bar{\psi}_{in} - \bar{\psi}_{out}]$$

$\lambda = -t + c$

$$\frac{d\lambda}{dt} = -1$$

$$-\frac{d\bar{\psi}}{d\lambda} = \frac{1}{t} [\bar{\psi}_{in}(\lambda) - \delta(\lambda)]$$

$$\frac{d\bar{\psi}}{d\lambda} = \frac{1}{t} [\delta(\lambda) - \bar{\psi}_{in}(\lambda)]$$

$$\text{Let: } \bar{\psi}_{in}(\lambda) = E(\lambda)$$

Then it follows from the relationship of I and E curves that

$$\bar{\psi} = I(\lambda)$$

### 3. Segregated Flow Model

$$m = 1, \quad \zeta_1 = \alpha, \quad \bar{\psi} = IC, \quad \bar{\psi}_{out} = EC$$

$$\frac{d}{d\alpha} \left( IC \frac{d\alpha}{dt} \right) + r(C)I = -\frac{Q}{V} EC$$

$$C \frac{dI}{d\alpha} + I \frac{dC}{d\alpha} + r(C)I = -\frac{Q}{V} EC$$

But since  $\frac{dI}{d\alpha} = -\frac{Q}{V} E$  the first term on the left hand side and the term on the right hand side

cancel out. The remaining terms yield the batch kinetics.

$$\frac{dC}{d\alpha} = -r(C)$$

$$\alpha = 0 \quad C = C_0$$

The exit concentration is given by

$$\bar{C} = \int_0^{\infty} C(\alpha) E(\alpha) d\alpha$$

### 4. Maximum Mixedness Model

$$m = 1, \quad \zeta_1 = \lambda, \quad \bar{\psi} = IC, \quad \bar{\psi}_{in} = EC_0$$

$$\frac{d}{d\lambda} \left( IC \frac{d\lambda}{dt} \right) + r(C)I = \frac{Q}{V} EC_0$$

$$I \frac{dC}{d\lambda} + \frac{Q}{V} E(C_0 - C) - r(C)I = 0$$

$$\frac{dC}{d\lambda} = r(C) - \frac{1}{\lambda} \frac{E}{I} (C_0 - C)$$

$$\lambda \rightarrow \infty \quad \frac{dC}{d\lambda} = 0$$

### 5. Unsteady State RTD (Evolution of RTD)

Both I and E are now two place functions: I ( $\alpha, t$ ) a function of fluid element age,  $\alpha$ , and actual time, t, and E ( $\alpha, t$ ), a function of fluid residence time,  $\alpha$ , and actual time, t. Hence,  $m = 1$ ,  $\zeta_1 = \alpha$ . Then from equation (2):

$$\frac{1}{V} \frac{\partial}{\partial t} (IV) + \frac{\partial}{\partial \alpha} (I) = [Q_{in} \delta(\alpha) - Q_{out} E(\alpha, t)]$$

Let  $V = \text{const}$ ,  $Q_{in} = Q_{out}$

Yet if state of the system is changed by some mechanism, the equation below describes the evolution of I ( $\alpha, t$ )

$$\frac{\partial I}{\partial t} + \frac{\partial I}{\partial \alpha} = \frac{1}{\bar{t}} [\delta(\alpha) - E(\alpha, t)]$$

$$t = 0 \quad I = I_o(\alpha) \quad E = E_o(\alpha)$$

Since in case of a CSTR,  $I = E$ , we can also write for a CSTR:

$$\frac{\partial E}{\partial t} + \frac{\partial E}{\partial \alpha} = \frac{1}{\bar{t}} [\delta(\alpha) - E] \quad (4)$$

By taking the Laplace Transform with respect to age  $\alpha$  of equation (4), so that

$$\bar{E}(s, t) = L\{E(\alpha, t)\} = \int_0^{\infty} E(\alpha, t) e^{-s\alpha} d\alpha, \text{ we get}$$

$$\frac{d\bar{E}}{dt} + s\bar{E} = \frac{1}{\bar{t}} [1 - \bar{E}]$$

$$\frac{d\bar{E}}{dt} + (s + \frac{1}{\bar{t}})\bar{E} = \frac{1}{\bar{t}}$$

$$\frac{d}{dt} \left( e^{(s+\frac{1}{\bar{t}})t} \bar{E} \right) = \frac{1}{\bar{t}} e^{(s+\frac{1}{\bar{t}})t}$$

$$e^{(s+\frac{1}{\bar{t}})t} \bar{E} - \bar{E}_o = \frac{1}{\bar{t}(s+\frac{1}{\bar{t}})} \left( e^{(s+\frac{1}{\bar{t}})t} - 1 \right)$$

$$\bar{E}(t, s) = \bar{E}_o(s) e^{-(s+\frac{1}{\bar{t}})t} + \frac{1}{\bar{t}(s+\frac{1}{\bar{t}})} \left[ 1 - e^{-(s+\frac{1}{\bar{t}})t} \right]$$

Upon inversion into the  $(\alpha, t)$  domain we get

$$E(t, \alpha) = e^{-t/\bar{t}} E_o(\alpha - t) + \frac{1}{\bar{t}} e^{-\alpha/\bar{t}} [H(\alpha) - H(\alpha - t)]$$

$$E_o(t, \alpha) = 0 \quad t > \alpha$$

$$\lim_{t \rightarrow \infty} E(t, \alpha) = \frac{1}{\bar{t}} e^{-\alpha/\bar{t}}$$

We could have instead used the Laplace transform in time on eq (4) with the following result:

$$s\bar{E} - E_o + \frac{d\bar{E}}{d\alpha} = \frac{1}{\bar{t}} \left[ \frac{\delta(\alpha)}{s} - \bar{E} \right]$$

$$\frac{d\bar{E}}{d\alpha} + (s + \frac{1}{\bar{t}})\bar{E} = \frac{1}{\bar{t}s} \delta(\alpha) + E_o(\alpha)$$

$$\frac{d}{d\alpha} \left( e^{+(s+\frac{1}{\bar{t}})\alpha} \bar{E} \right) = \frac{1}{\bar{t}s} \delta(\alpha) e^{+(s+\frac{1}{\bar{t}})\alpha} + E_o(\alpha) e^{+(s+\frac{1}{\bar{t}})\alpha}$$

$$e^{+(s+\frac{1}{\bar{t}})\alpha} \bar{E} = \frac{1}{\bar{t}s} H(\alpha) + \int_0^{\alpha} E_o(\alpha') e^{+(s+\frac{1}{\bar{t}})\alpha'} d\alpha'$$

$$\bar{E}(s, \alpha) = \frac{1}{\bar{t}s} e^{-(s+\frac{1}{\bar{t}})\alpha} H(\alpha) + \int_0^{\alpha} E_o(\alpha') e^{-(s+\frac{1}{\bar{t}})(\alpha-\alpha')} d\alpha'$$

Inversion into the  $(t, \alpha)$  domain produces:

$$\begin{aligned}
 E(t, \alpha) &= \frac{1}{t} e^{-\frac{\alpha}{t}} H(t - \alpha) H(\alpha) + \int_0^{\alpha} E_o(\alpha') e^{-\frac{1}{t}(\alpha - \alpha')} \delta(t - (\alpha - \alpha')) d\alpha' \\
 &= \frac{1}{t} e^{-\frac{\alpha}{t}} H(t - \alpha) H(\alpha) + E_o(\alpha - t) e^{-t/t} \\
 &= e^{-t/t} E_o(\alpha - t) + \frac{1}{t} e^{-\frac{\alpha}{t}} [H(\alpha) - H(\alpha - t)]
 \end{aligned}$$

Of course the same final result is obtained.